

Guided-Wave, Electro-Optic Electric-Field Sensors Utilizing Ti Diffused Lithium-Niobate (Ti:LiNbO₃) Channel Waveguides

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ABSTRACT

This paper comprehensively reviews and compares Ti:LiNbO₃ integrated optic electric-field sensors, including the asymmetric Mach-Zehnder interferometer (MZI), 1 × 2 directional coupler (DC), and Y-fed balanced-bridge Mach-Zehnder interferometer (YBB-MZI), based on the operating principles, the dc/ac electrical and optical characteristics, and electric-field measurements for each fabricated device, respectively.

Keywords: integrated-optics, electric-field sensor, electro-optic effect, Ti:LiNbO₃ channel waveguide,

1. INTRODUCTION

Electro-optic electric-field sensors utilizing Ti:LiNbO₃ channel waveguides, being all-dielectric, present several intrinsic advantages compared to their electronic counterparts, such as noise immunity, compact size (a few millimeters), large bandwidth, feasibility of electrode-free operation, and consequently the possibility of operating even in harsh or dangerous environments. The optical fibers and dielectric electro-optic materials also produce minimal field distortion. In this paper we review and compare Ti:LiNbO₃ E-field sensors based on the electro-optic effect of lithium-niobate. Three types of E-field sensors were reviewed according to configurations, operating principles, fabrication, dc/ac characteristics, and various experimental results including E-field-sensed RF spectra, and frequency responses. [1]

2. FABRICATION and DEVICE THEORY and STRUCTURES

2.1 Fabrication of Ti:LiNbO₃ channel waveguide

The integrated-optic sensors were fabricated on X- or Z-cut LiNbO₃ substrate using standard photolithographic technique. Channel waveguides were formed by diffusing a 1050-Å-thick, 7.5μm-wide stripe of titanium film at 1050°C in wet ambient. The substrate edges were optically polished to allow butt coupling and pig-tailing. A SiO₂ buffer layer ~3000 Å thick was deposited using e-beam evaporation and 99.99% pure SiO₂ pellets to prevent propagation loss caused by the optical absorption of the antenna metal. An aluminium dipole antenna electrode ~5000 Å thick was fabricated to allow sensing of the electric field. [1] Polarization maintaining single-mode and multi-mode optical fibers were attached to the input and output waveguides, respectively.

2.2 Asymmetric Mach-Zehnder Interferometer

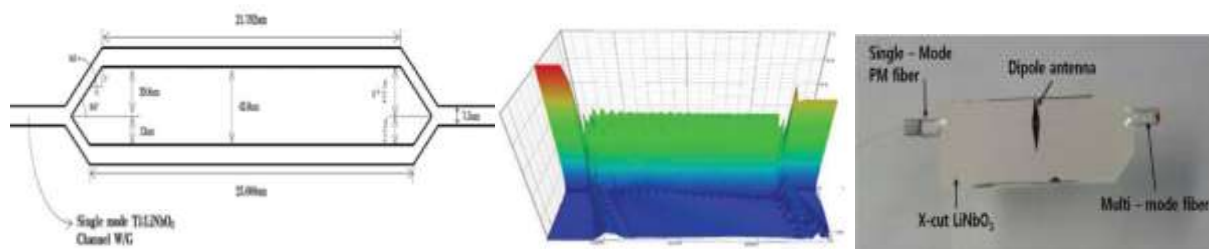


Fig. 1 (a) Schematic diagrams and dimensions, (b) BPM-CAD simulations, and (c) fabricated sensor module of Ti:LiNbO₃ asymmetric Mach-Zehnder interferometer.

A configuration of an asymmetric Ti:LiNbO₃ Mach-Zehnder interferometer and optical propagation BPM-CAD simulations are shown in Fig. 1. [2] The device was designed to have $\pi/2$ phase difference between its two arms through adjusting the path length difference, which makes the sensor have better linearity and sensitivity without a need for external bias to be applied. The device has a 3-dB input splitter and output combiner. The sensed E-field produces phase shifts in the light beam propagating in one of the parallel channel waveguide arms, thereby leading to a net phase shift between two light beams through each channel. When the two light beams recombine

at the output combiner, the phase modulation is converted to an amplitude-modulated signal at the same frequency as the sensed E-field. Therefore the light signal amplitude is proportional to the E-field strength.

2.3 1×2 Directional Coupler

A 1 × 2 directional coupler consists of a single-mode Y-junction splitter and a co-directional coupler with two parallel and symmetric waveguide channels. [3] The schematic diagram and its dimensions are shown in Fig. 2. Light is fed in and split into the two symmetric waveguides equally through the Y-junction region. The co-directional coupler guides the two single-mode light beams traveling along the two channels. With no modulating voltage applied, the coupler is set to the 3-dB operating point automatically due to the symmetric structure of the 1 × 2 directional coupler. While a driving voltage is applied through the electrodes over the coupler region, however, light can be coupled from one channel into the other. The 1 × 2 directional coupler modulator has two complementary optical outputs and, in general, is characterized by its interaction length (L), coupling conversion length (lc), and the phase mismatch of the propagation constant ($\Delta\beta$) between the two arms.

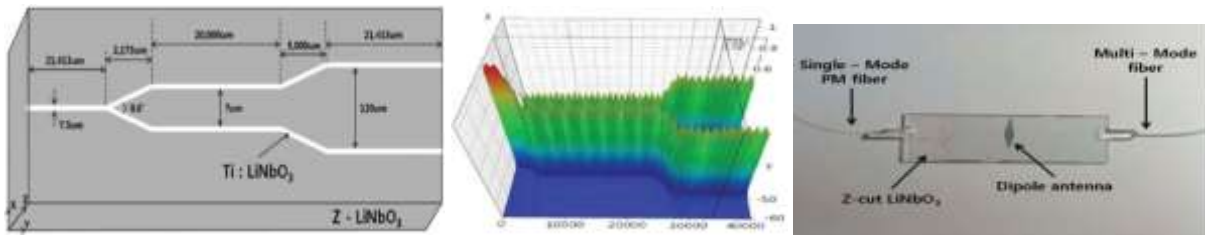


Fig. 2. (a) Schematic diagrams and dimensions, (b) BPM-CAD simulations, and (c) fabricated sensor module of Ti:LiNbO₃ 1×2 directional coupler.

2.4 1×2 Y-fed balanced bridge Mach-Zehnder interferometer

The YBB-MZI modulator consists of a 3-dB directional coupler at the output and has two complementary output waveguide as shown in Fig. 3. [4] This type of modulator provides a well-defined transfer function for the output optical power versus the detected electric-field intensity and can be automatically biased at the optimum 3 dB operating point due to its symmetrical structure, which offers a more tolerant design in the fabrication process than Mach-Zehnder interferometric modulators or 1 × 2 directional couplers, which are asymmetrical.

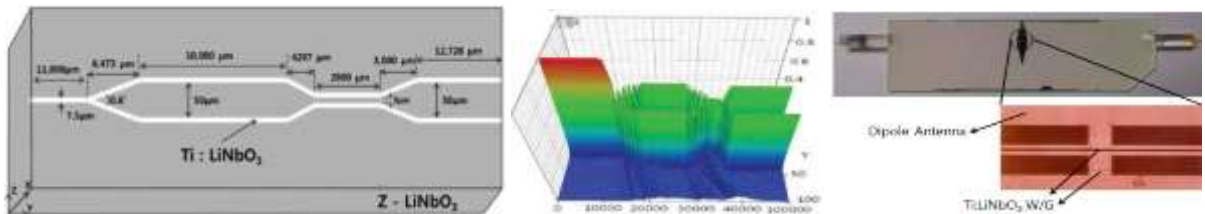


Fig. 3. (a) Schematic diagrams and dimensions, (b) BPM-CAD simulations, and (c) fabricated sensor module of Ti:LiNbO₃ 1×2 YBB-MZI interferometer.

3. DC/AC CHARACTERISTICS and E-FIELD SENSING

3.1 DC Characteristic Curve

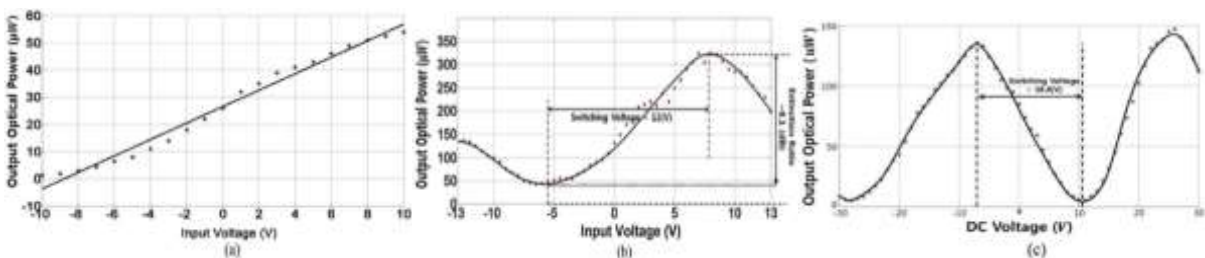


Fig. 5. Measured optical output power intensities versus applied dc voltage of (a) asymmetric Mach-Zehnder interferometer, (b) 1 × 2 directional coupler, and (c) 1 × 2 YBB-MZI interferometer.

3.2 AC Characteristics

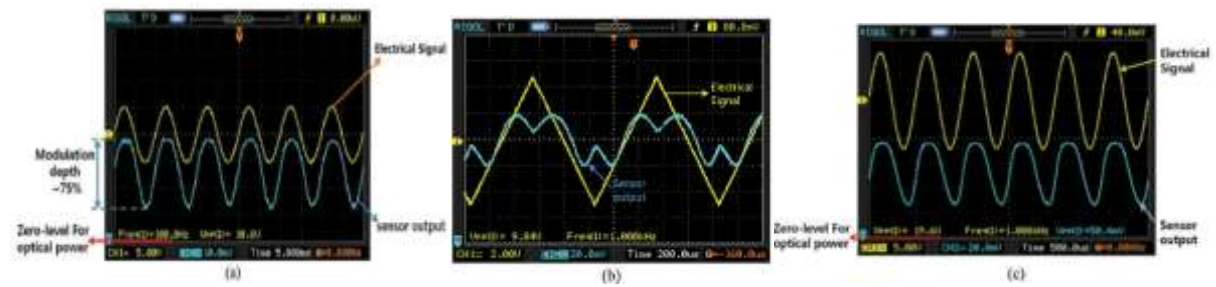


Fig. 6. The 1-kHz ac modulation responses of (a) asymmetric Mach-Zehnder interferometer, (b) 1×2 directional coupler, and (c) 1×2 YBB-MZI interferometer.

3.3 RF Sensing

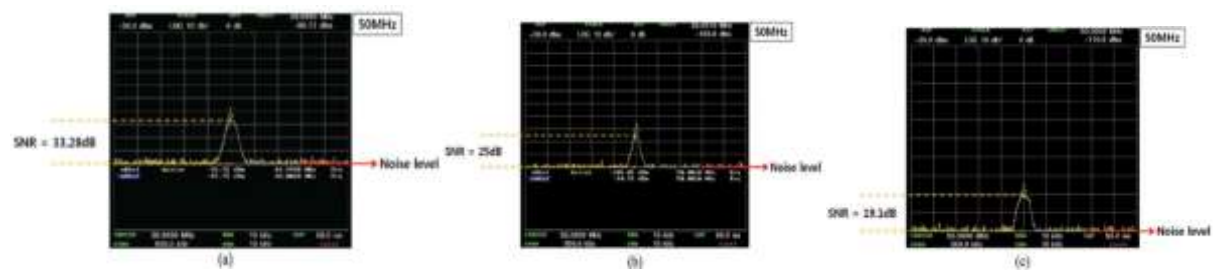


Fig. 7. The RF spectra of 50 MHz RF input signal into the TEM cell with a power level of 100 mW: (a) asymmetric Mach-Zehnder interferometer, (b) 1×2 directional coupler, and (c) 1×2 YBB-MZI interferometer.

4. CONCLUSIONS

The ac output characteristics of the asymmetric MZI interferometer show a modulation depth of $\sim 75\%$ at $V\pi$ voltage of ~ 5.3 V. The minimum detectable electric fields are ~ 0.28 V/m and ~ 0.646 V/m, corresponding to a dynamic range of about ~ 32 dB and ~ 26 dB at frequencies of 20 MHz and 50 MHz, respectively. A dc switching voltage of ~ 12 V and an extinction ratio of ~ 8.1 dB were observed with the 1×2 directional coupler. The minimum detectable electric fields are ~ 0.99 V/m and ~ 1.67 V/m, corresponding to a dynamic range of about ~ 29.5 dB and ~ 25 dB at frequencies of 20 MHz and 50 MHz, respectively. A dc switching voltage of ~ 16.6 V and an extinction ratio of ~ 14.7 dB were observed on the 1×2 YBB-MZI interferometer. The minimum detectable electric fields are ~ 1.12 V/m and ~ 3.3 V/m, corresponding to a dynamic range of about ~ 22 dB and ~ 18 dB at frequencies of 10 MHz and 50 MHz, respectively.

ACKNOWLEDGEMENTS

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REFERENCES

- [1] H. S. Jung: Ti:LiNbO₃ Integrated Optic Electric-Field Sensors based on Electro-Optic Effect, *Fiber and Integrated Optics*, vol. 35(3) pp. 161-180, Jun. 2016.
- [2] H. S. Jung: Photonic electric-field sensor utilizing an asymmetric Ti: LiNbO₃ Mach-Zehnder interferometer with a dipole antenna, *Fiber and Integrated Optics*, vol. 31(6) pp. 343–354, Dec.2012.
- [3] H. S. Jung: Electro-optic electric-field sensors utilizing Ti: LiNbO₃ 1×2 directional coupler with dipole antennas, *Optical Engineering*, vol. 52(6) pp. 064402.1–064402.6, June 2013.
- [4] H. S. Jung: An Integrated Photonic Electric-Field Sensor Utilizing a 1×2 YBB Mach-Zehnder Interferometric Modulator with a Titanium-Diffused Lithium Niobate Waveguide and a Dipole Patch Antenna, *Crystals*, vol. 9(9) pp. 459(1-11), Sep. 2019.